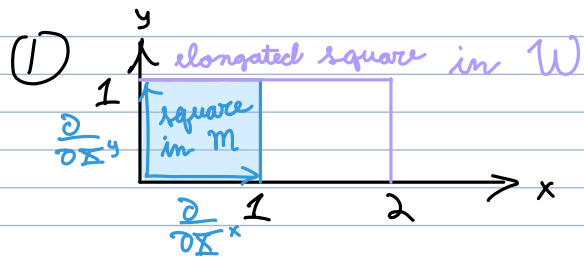


13. HW 3 : Elasticity

Continuous Theory

① 2D Square Elongation
(youtube example)

- Calculate the deformation gradient F of a 2D square that has been elongated by twice its length along one of its dimensions.



$$M \xrightarrow{\phi} W$$

$$\frac{\partial}{\partial X^a} \quad \frac{\partial}{\partial x^i}$$

$$\vec{x} = \phi(\vec{X}) = \begin{bmatrix} 2X^x \\ X^y \end{bmatrix}$$

$$F = \frac{\partial \phi^i}{\partial X^a} = \begin{bmatrix} \frac{\partial 2X^x}{\partial X^x} & \frac{\partial 2X^x}{\partial X^y} \\ \frac{\partial X^y}{\partial X^x} & \frac{\partial X^y}{\partial X^y} \end{bmatrix}$$

$$= \begin{bmatrix} 2 & 0 \\ 0 & 1 \end{bmatrix}$$

② 3D Abstract Time-Dependent Motion (youtube ex.)

- Calculate F from the following flow map ϕ .

$$\phi(\vec{X}, t) = \begin{bmatrix} 3X^x X^y + tX^z \\ X^y - tX^x \\ 5X^y X^z \end{bmatrix}$$

② Assume:

$$\phi(\vec{X}, t) = \begin{bmatrix} 3X^x X^y + tX^z \\ X^y - tX^x \\ 5X^y X^z \end{bmatrix}$$

$$F = \frac{\partial \phi^i}{\partial X^a} = \begin{bmatrix} \frac{\partial}{\partial X^x} & \frac{\partial}{\partial X^y} & \frac{\partial}{\partial X^z} \\ \frac{\partial}{\partial X^x} & \frac{\partial}{\partial X^y} & \frac{\partial}{\partial X^z} \\ \frac{\partial}{\partial X^x} & \frac{\partial}{\partial X^y} & \frac{\partial}{\partial X^z} \end{bmatrix}$$

$$= \begin{bmatrix} 6X^x X^y & 3X^x X^z & 3tX^z \\ -t & 0 & 2X^z \\ 0 & 5X^z & 5X^y \end{bmatrix}$$

- F may not be symmetric.
- F is a fn of \vec{X} and t .

Discrete Theory

① What are the steps involved in doing an elastic body simulation based on the Piola stress tensor framework?

Note: the subscript "c" means "per cell" and the subscript "v" means "per vertex".

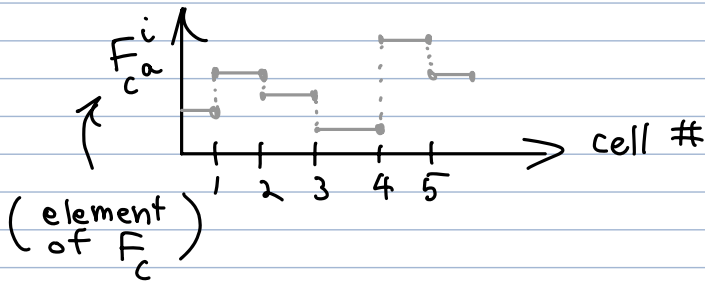
Equivalent approach:

$$C_c \rightarrow U_c \rightarrow U_{tot} = \sum_c U_c$$

$$f = \frac{\partial U_{tot}}{\partial x_i}$$

② Calculate F_c for a 2D mesh.

Note: We have a different F_c for each cell. Thus, F_c^i is piecewise constant.



① (i) $\phi(\vec{X}) = \vec{x}_v$ (flow map)

(ii) F_c (deformation grad.)

(iii) $C_c = F_c^T F_c$ (induced metric)

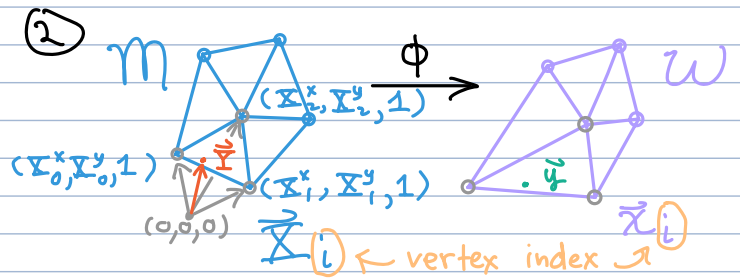
(iv) $E_c = \frac{1}{2} (C_c - I)$ (strain tensor)

(v) Find appropriate stress-strain relation. One possible choice:
 $S_c = 2\mu E_c + \lambda \text{tr}(E_c) I$ (1st Piola stress)

(vi) $P_c = F S_c$ (1st Piola stress = $\frac{\partial U}{\partial F}$)

(vii) $\vec{F}_v = \frac{1}{n} \sum_{c \ni v} P_c \hat{n}_{c,v} A_{c,v}$
 (= $\text{div}(P_c)$ = discrete divergence)

(ix) $\vec{v}_v = \vec{F}_v / m_v$, $\dot{\vec{X}}_v = \vec{v}_v$



$\vec{x}_i = \phi(\vec{X}_i)$ is the discrete (finite-dimensional) flow map.

$\vec{y} = \phi(\vec{Y})$ is the continuous (infinite-dimensional) flow map.

$$F_c = \frac{\partial \phi^i}{\partial Y^a}$$

$i \leftarrow$ increment over $\dim(\mathcal{W}) = 2$
 $a \leftarrow$ increment over $\dim(\mathcal{M}) = 2$

$$\text{Given } \begin{bmatrix} y^x \\ y^y \\ 1 \end{bmatrix} = \phi_c(\vec{Y}) = AB \begin{bmatrix} Y^x \\ Y^y \\ 1 \end{bmatrix}$$

$$A = \begin{bmatrix} x_0^x & x_1^x & x_2^x \\ x_0^y & x_1^y & x_2^y \\ 1 & 1 & 1 \end{bmatrix}$$

$$B = \begin{bmatrix} x_0^x & x_1^x & x_2^x \\ x_0^y & x_1^y & x_2^y \\ 1 & 1 & 1 \end{bmatrix}^{-1}$$

$$Q = AB = \begin{bmatrix} \rho_{11} & \rho_{12} & \rho_{13} \\ \rho_{21} & \rho_{22} & \rho_{23} \\ \rho_{31} & \rho_{32} & \rho_{33} \end{bmatrix}$$

we care about this part:

$$\therefore \phi_c(\vec{Y}) = \left[\begin{array}{c} \boxed{Q_a^x Y^x + Q_b^x Y^y} + Q_c^x \\ Q_a^y Y^x + Q_b^y Y^y + Q_c^y \\ Q_d^x Y^x + Q_e^x Y^y + Q_f^x \\ Q_d^y Y^x + Q_e^y Y^y + Q_f^y \end{array} \right] \downarrow i$$

$$F_c = \frac{\partial \phi_c^i}{\partial Y^a} = \begin{bmatrix} Q_a^x & Q_b^x \\ Q_a^y & Q_b^y \end{bmatrix} \quad \begin{array}{l} i = 0, 1 \\ a = 0, 1 \end{array}$$

(per cell)

Alternative approach for getting F_c (produces equivalent result):

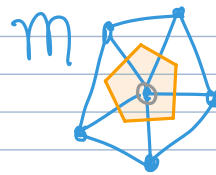
$$F_c = -\frac{1}{nV_c} \sum_{j=0}^5 \begin{bmatrix} x_j^i \\ r_j \end{bmatrix} [-A_{c,j} n_{j,j}^T]$$

We use this to derive our discrete divergence operator in $\vec{f}_v = \text{div}(P_c)$.

③ Calculate m_v .

Note: ρ is the mass density.

$$\textcircled{3} \quad m_v = \rho \sum_{c \in V} \frac{1}{n+1} V_c$$



m_v is a diagonal matrix (which makes matrix inversion easier).

References

- (1) Chern, Albert. CSE 291 course Notes, Spring 2024.
- (2) Zubov, L. M. "Variational Principles of the Nonlinear Theory of Elasticity," Journal of Applied Mathematics and Mechanics, 35, 3, 406-410, 1971.